

2A, 23V, 340kHz Synchronous Step-Down Converter

General Description

The RT8284N is a high-efficiency monolithic synchronous step-down DC/DC converter that can deliver up to 2A output current from a 4.5V to 23V input supply. The RT8284N current mode architecture and external compensation allow the transient response to be optimized over a wide range of loads and output capacitors. Cycle-by-cycle current limit provides protection against shorted outputs and soft-start eliminates input current surge during start-up. The RT8284N also provide under voltage protection and thermal shutdown protection. The low current ($< 3\mu\text{A}$) shutdown mode provides output disconnect, enabling easy power management in battery-powered systems. The RT8284N is available in a SOP-8 and SOP-8 (Exposed Pad) package.

Ordering Information

RT8284N	□	□
	Package Type	
	S : SOP-8	
	SP: SOP-8(Exposed Pad-Option 1)	
	Operating Temperature Range	
	G : Green (Halogen Free with Commercial Standard)	

Note :

Richtek Green products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

Features

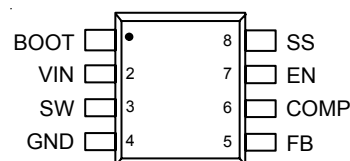
- $\pm 1.5\%$ High Accuracy Feedback Voltage
- Input Voltage Range : 4.5V to 23V
- 2A Output Current
- Integrated N-Channel MOSFETs
- Current Mode Control
- 340kHz Fixed Frequency Operation
- Output Adjustable Voltage Range : 0.923V to 20V
- Efficiency Up to 95%
- Programmable Soft-Start
- Stable with Low ESR Ceramic Output Capacitors
- Cycle-by Cycle Over Current Protection
- Input Under Voltage Lockout
- Output Under Voltage Protection
- Thermal Shutdown Protection
- RoHS Compliant and Halogen Free

Applications

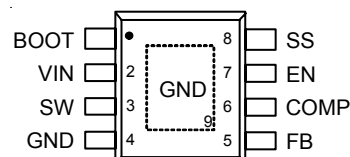
- Wireless AP/Router
- Set-Top-Box
- Industrial and Commercial Low Power Systems
- LCD Monitors and TVs
- Green Electronics/Appliances
- Point of Load Regulation of High-Performance DSPs

Pin Configurations

(TOP VIEW)



SOP-8



SOP-8 (Exposed Pad)

RT8284N

Marking Information

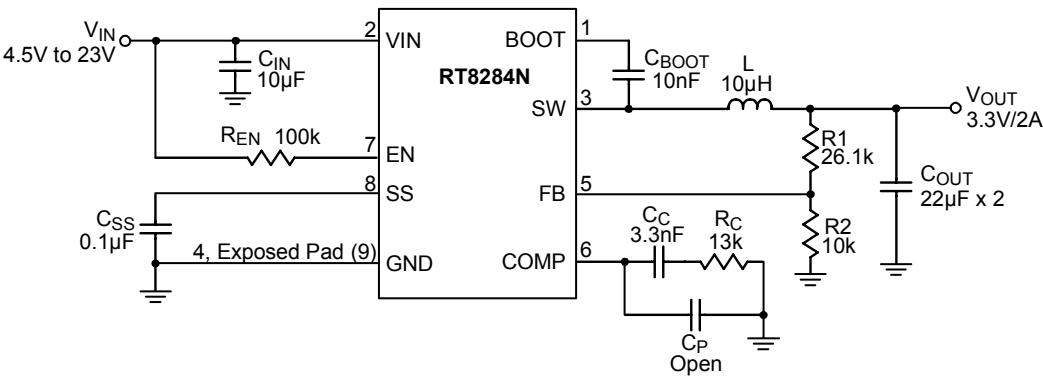
RT8284N
GSYMDNN

RT8284NGS : Product Number
YMDNN : Date Code

RT8284N
GSPYMDNN

RT8284NGSP : Product Number
YMDNN : Date Code

Typical Application Circuit



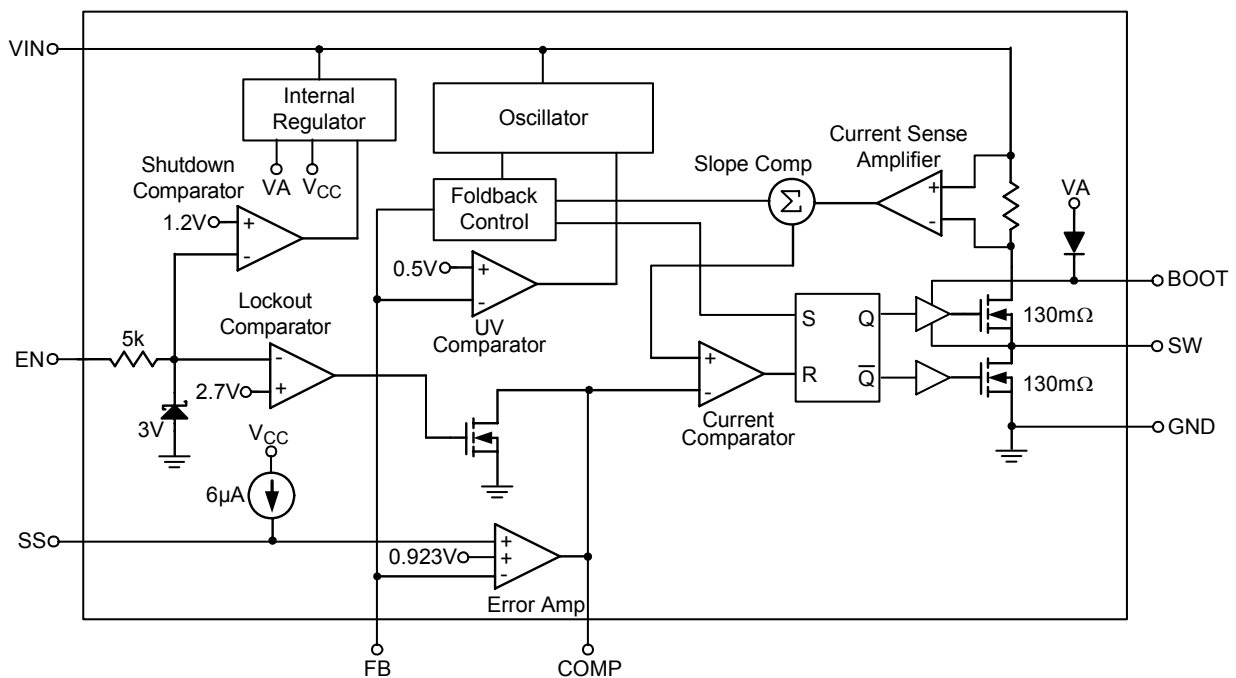
Recommended Component Selection

V_{OUT} (V)	R_1 (k Ω)	R_2 (k Ω)	R_C (k Ω)	C_C (nF)	L (μ H)	C_{OUT} (μ F)
8	76.8	10	27	3.3	22	22 x 2
5	45.3	10	20	3.3	15	22 x 2
3.3	26.1	10	13	3.3	10	22 x 2
2.5	16.9	10	9.1	3.3	6.8	22 x 2
1.8	9.53	10	5.6	3.3	4.7	22 x 2
1.2	3	10	3.6	3.3	3.6	22 x 2

Functional Pin Description

Pin No.		Pin Name	Pin Function
SOP-8 (Exposed Pad)	SOP-8		
1	1	BOOT	Bootstrap for High-Side Gate Driver. Connect a 10nF or greater ceramic capacitor from BOOT to SW pins.
2	2	VIN	Input Supply Voltage, 4.5V to 23V. Must bypass with a suitably large ceramic capacitor.
3	3	SW	Phase Node. Connect this pin to external L-C filter.
4, 9 (Exposed Pad)	4	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.
5	5	FB	Feedback Input Pin. This pin is connected to the converter output. It is used to set the output of the converter to regulate to the desired value via an internal resistive divider. For an adjustable output, an external resistive divider is connected to this pin.
6	6	COMP	Compensation Node. COMP is used to compensate the regulation control loop. Connect a series RC network from COMP to GND. In some cases, an additional capacitor from COMP to GND is required.
7	7	EN	Enable Input pin. A logic high enables the converter; a logic low force the RT8284N into shutdown mode reducing the supply current to less than 3 μ A. Attach this pin to VIN with a 100k Ω pull up resistor for automatic startup.
8	8	SS	Soft-Start Control Input. SS controls the soft-start period. Connect a capacitor from SS to GND to set the soft-start period. A 0.1 μ F capacitor sets the soft-start period to 15.5ms .

Function Block Diagram



RT8284N

Absolute Maximum Ratings (Note 1)

- Supply Voltage, V_{IN} ----- -0.3V to 25V
- Input Voltage, SW ----- -0.3V to ($V_{IN} + 0.3V$)
- $V_{BOOT} - V_{SW}$ ----- -0.3V to 6V
- Other Pins Voltages ----- -0.3V to 6V
- Power Dissipation, P_D @ $T_A = 25^\circ C$
 - SOP-8 ----- 1.111W
 - SOP-8 (Exposed Pad) ----- 1.333W
- Package Thermal Resistance (Note 4)
 - SOP-8, θ_{JA} ----- $90^\circ C/W$
 - SOP-8 (Exposed Pad), θ_{JA} ----- $75^\circ C$
 - SOP-8 (Exposed Pad), θ_{JC} ----- $15^\circ C$
- Junction Temperature ----- $150^\circ C$
- Lead Temperature (Soldering, 10 sec.) ----- $260^\circ C$
- Storage Temperature Range ----- $-40^\circ C$ to $150^\circ C$
- ESD Susceptibility (Note 2)
 - HBM (Human Body Mode) ----- 2kV
 - MM (Machine Mode) ----- 200V

Recommended Operating Conditions (Note 3)

- Supply Voltage, V_{IN} ----- 4.5V to 23V
- Junction Temperature Range ----- $-40^\circ C$ to $125^\circ C$
- Ambient Temperature Range ----- $-40^\circ C$ to $85^\circ C$

Electrical Characteristics

($V_{IN} = 12V$, $T_A = 25^\circ C$ unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Shutdown Supply Current		$V_{EN} = 0V$	--	0.5	3	μA
Supply Current	I_{CC}	$V_{EN} = 3V$, $V_{FB} = 1V$	--	0.8	1.2	mA
Feedback Voltage	V_{FB}	$4.5V \leq V_{IN} \leq 23V$	0.909	0.923	0.937	V
Error Amplifier Transconductance	G_{EA}	$\Delta I_C = \pm 10\mu A$	--	940	--	$\mu A/V$
High-Side Switch-On Resistance	$R_{DS(ON)1}$		--	130	--	m Ω
Low-Side Switch-On Resistance	$R_{DS(ON)2}$		--	130	--	m Ω
High-Side Switch Leakage Current		$V_{EN} = 0V$, $V_{SW} = 0V$	--	0	10	μA
Upper Switch Current Limit		Min.Duty Cycle, $V_{BOOT-SW} = 4.8V$	--	4.5	--	A
Low Switch Current Limit		From Drain to Source	--	1.2	--	A
COMP to Current Sense Transconductance	G_{CS}		--	5	--	A/V
Oscillator Frequency	f_{OSC1}		300	340	380	kHz
Short Circuit Oscillation Frequency	f_{OSC2}	$V_{FB} = 0V$	--	110	--	kHz
Maximum Duty Cycle	D_{MAX}	$V_{FB} = 0.7V$	--	93	--	%
Minimum On-Time	t_{ON}		--	100	--	ns

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
EN Threshold Voltage	Logic High	V_{IH}		2.7	--	5.5	V
	Logic Low	V_{IL}		--	--	0.4	
Input Under Voltage Lockout Threshold			V_{IN} Rising	3.8	4.2	4.5	V
Input Under Voltage Lockout Hysteresis				--	320	--	mV
Soft-Start Current			$V_{SS} = 0V$	--	6	--	μA
Soft-Start Period			$C_{SS} = 0.1\mu F$	--	15.5	--	ms
Thermal Shutdown		T_{SD}		--	150	--	$^{\circ}C$

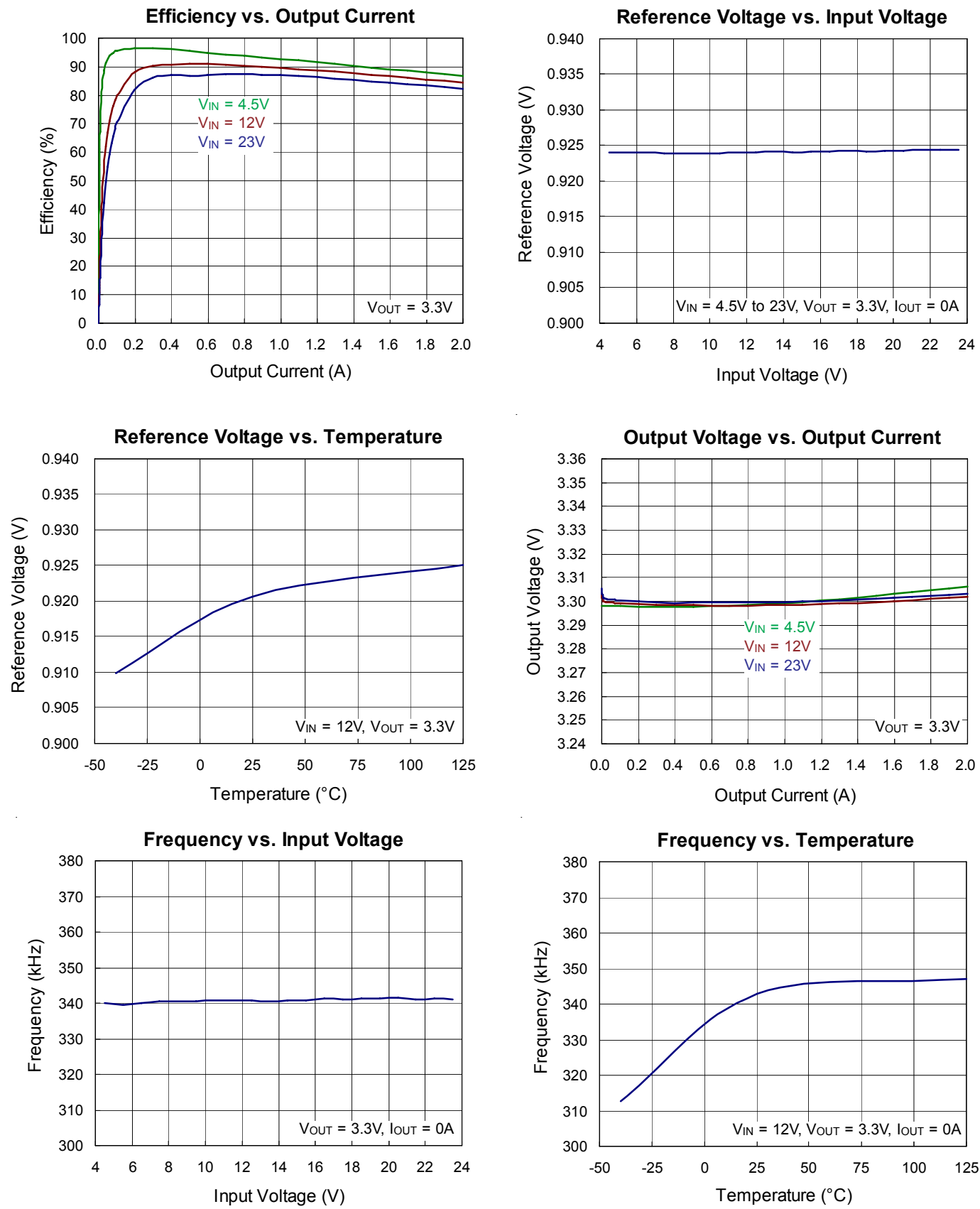
Note 1. Stresses listed as the above "Absolute Maximum Ratings" may cause permanent damage to the device. These are for stress ratings. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may remain possibility to affect device reliability.

Note 2. Devices are ESD sensitive. Handling precaution is recommended.

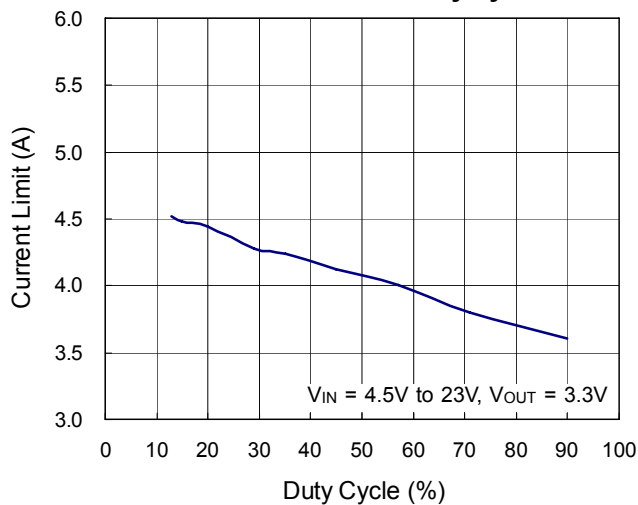
Note 3. The device is not guaranteed to function outside its operating conditions.

Note 4. θ_{JA} is measured in natural convection at $T_A = 25^{\circ}C$ on a high-effective thermal conductivity four-layer test board, refer to JEDEC 51-7 thermal measurement standard. The measurement case position of θ_{JC} is on the exposed pad for SOP-8 (Exposed Pad) package.

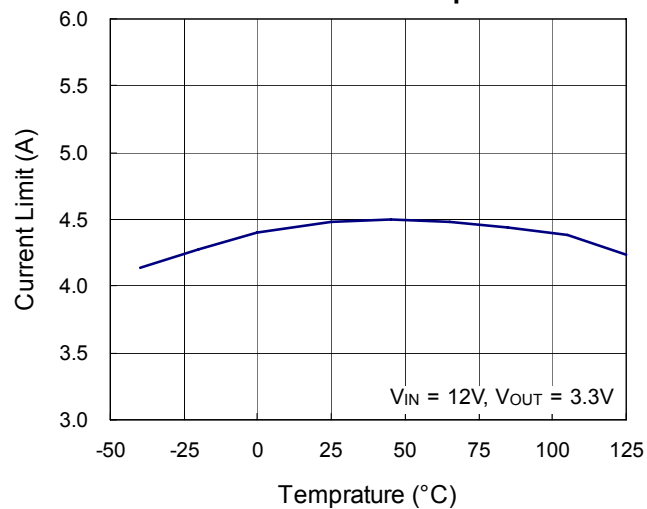
Typical Operating Characteristics



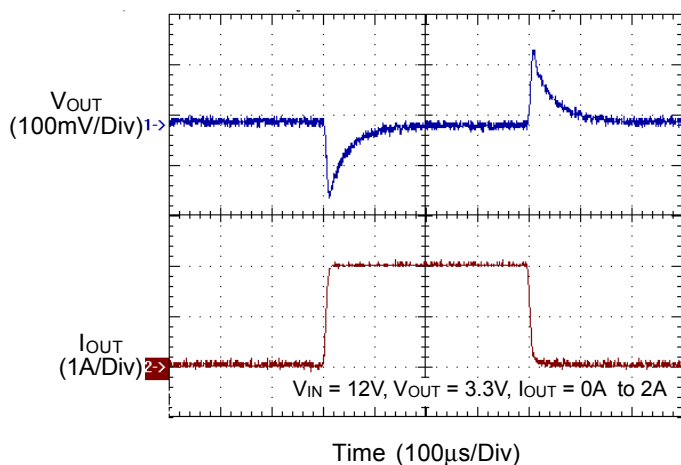
Current Limit vs. Duty cycle



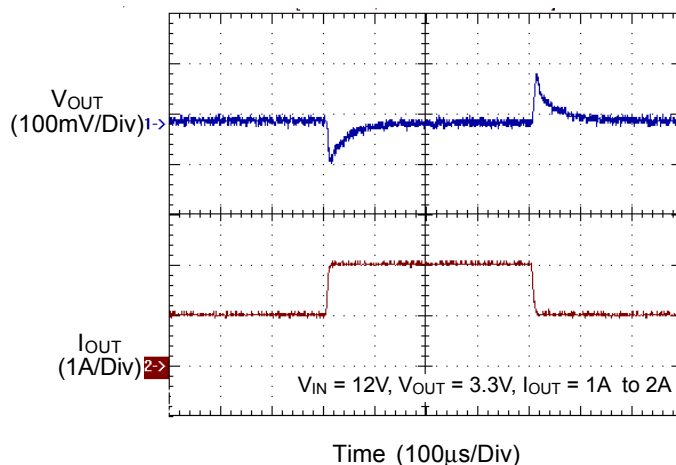
Current Limit VS. Temperature



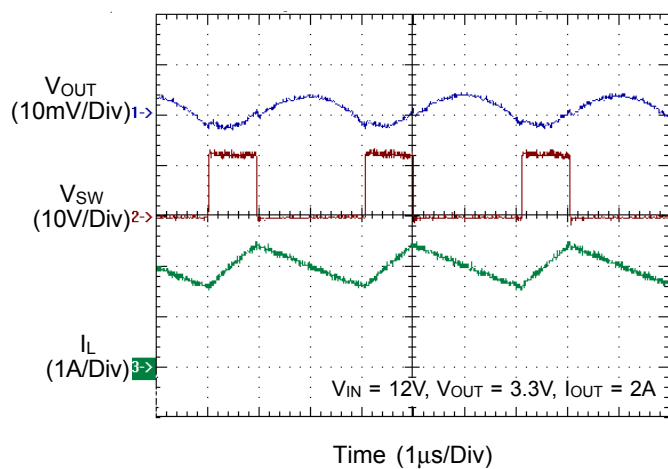
Load Transient Response



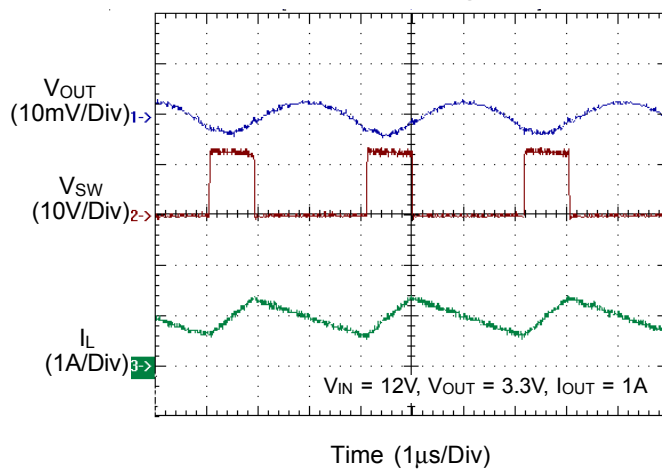
Load Transient Response



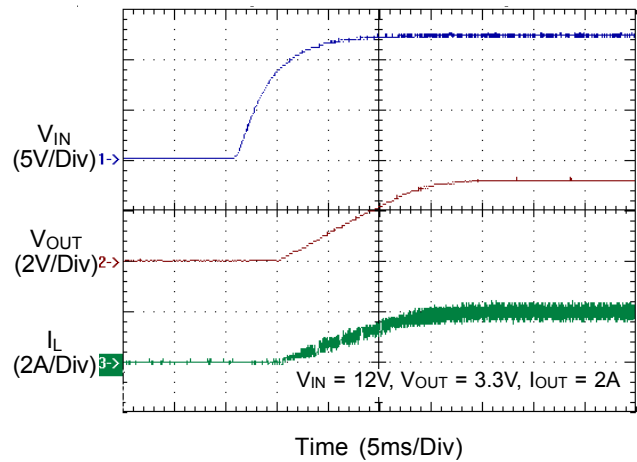
Switching



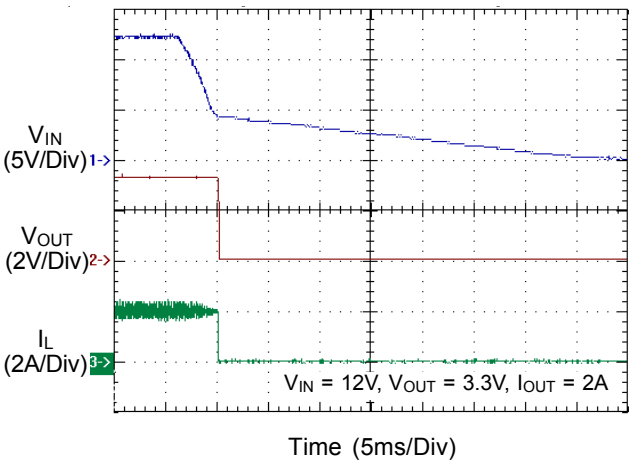
Switching



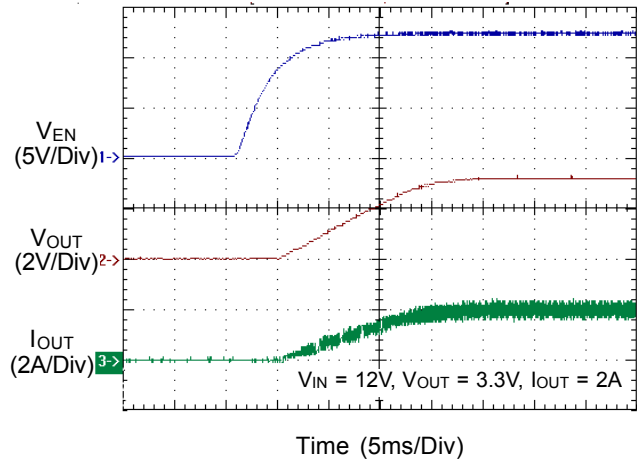
Power On from VIN



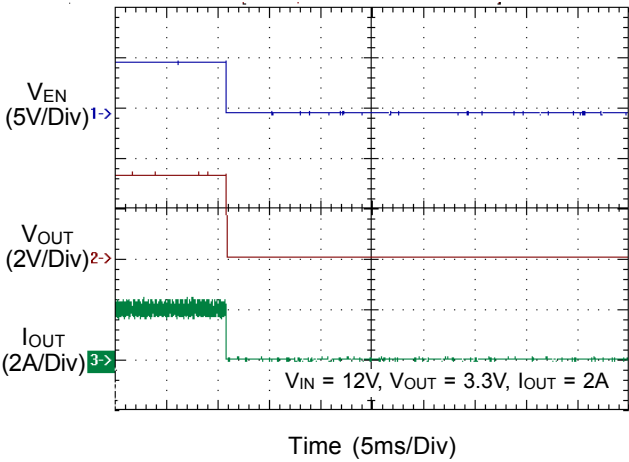
Power Off from VIN



Power On from EN



Power Off from EN



Application Information

The RT8284N is a synchronous high voltage buck converter which can support the input voltage range from 4.5V to 23V and the output current can be up to 2A.

Output Voltage Setting

The resistive divider allows the FB pin to sense the output voltage as shown in Figure 1.

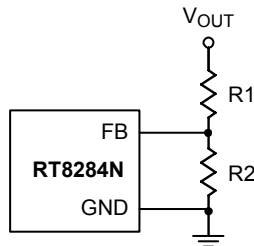


Figure 1. Output Voltage Setting

The output voltage is set by an external resistive voltage divider according to the following equation :

$$V_{OUT} = V_{FB} \left(1 + \frac{R1}{R2} \right)$$

Where V_{FB} is the feedback reference voltage 0.923V (typ.).

External Bootstrap Diode

Connect a 10nF low ESR ceramic capacitor between the BOOT pin and SW pin. This capacitor provides the gate driver voltage for the high side MOSFET.

It is recommended to add an external bootstrap diode between an external 5V and BOOT pin for efficiency improvement when input voltage is lower than 5.5V or duty ratio is higher than 65% .The bootstrap diode can be a low cost one such as IN4148 or BAT54. The external 5V can be a 5V fixed input from system or a 5V output of the RT8284N. Note the external boot voltage must be lower than 5.5V

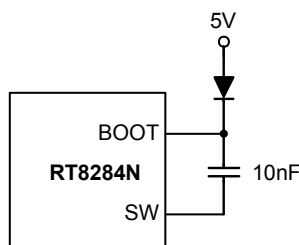


Figure 2. External Bootstrap Diode

Soft-Start

The RT8284N contains an external soft-start clamp that gradually raises the output voltage. The soft-start timing can be programmed by the external capacitor between SS pin and GND. The chip provides a 6μA charge current for the external capacitor. If 0.1μF capacitor is used to set the soft-start, it's period will be 15.5ms (typ.).

Chip Enable Operation

The EN pin is the chip enable input. Pull the EN pin low (<0.4V) will shutdown the device. During shutdown mode, the RT8284N quiescent current drops to lower than 3μA. Drive the EN pin to high (> 2.7V, < 5.5V) will turn on the device again. For external timing control (e.g.RC), the EN pin can also be externally pulled to High by adding a R_{EN} * resistor and C_{EN} *capacitor from the VIN pin (see Figure 3).

Hiccup Mode

For the RT8284N, it provides hiccup mode Under Voltage Protection (UVP). When the FB voltage drops below 0.5V, V_{FB} , the UVP function will be triggered and the RT8284N will shut down for a period of time and then recover automatically. The Hiccup Mode UVP can reduce input current in short-circuit conditions.

Inductor Selection

The inductor value and operating frequency determine the ripple current according to a specific input and output voltage. The ripple current ΔI_L increases with higher V_{IN} and decreases with higher inductance.

$$\Delta I_L = \left[\frac{V_{OUT}}{f \times L} \right] \times \left[1 - \frac{V_{OUT}}{V_{IN}} \right]$$

Having a lower ripple current reduces not only the ESR losses in the output capacitors but also the output voltage ripple. High frequency with small ripple current can achieve highest efficiency operation. However, it requires a large inductor to achieve this goal.

For the ripple current selection, the value of $\Delta I_L = 0.24(I_{MAX})$ will be a reasonable starting point. The largest ripple current occurs at the highest V_{IN} . To guarantee that the ripple current stays below the specified maximum, the

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inductor value should be chosen according to the following equation :

$$L = \left[\frac{V_{OUT}}{f \times \Delta I_L(MAX)} \right] \times \left[1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right]$$

The inductor's current rating (caused a 40°C temperature rising from 25°C ambient) should be greater than the maximum load current and its saturation current should be greater than the short circuit peak current limit. Please see Table 2 for the inductor selection reference.

Table 2. Suggested Inductors for Typical Application Circuit

Component Supplier	Series	Dimensions (mm)
TDK	VLF10045	10 x 9.7 x 4.5
TDK	SLF12565	12.5 x 12.5 x 6.5
TAIYO YUDEN	NR8040	8 x 8 x 4

C_{IN} and C_{OUT} Selection

The input capacitance, C_{IN}, is needed to filter the trapezoidal current at the source of the high side MOSFET. To prevent large ripple current, a low ESR input capacitor sized for the maximum RMS current should be used. The RMS current is given by :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at V_{IN} = 2V_{OUT}, where I_{RMS} = I_{OUT}/2. This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief.

Choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design.

For the input capacitor, one 10μF low ESR ceramic capacitors are recommended. For the recommended capacitor, please refer to table 3 for more detail.

The selection of C_{OUT} is determined by the required ESR to minimize voltage ripple.

Moreover, the amount of bulk capacitance is also a key for C_{OUT} selection to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section.

The output ripple, ΔV_{OUT}, is determined by :

$$\Delta V_{OUT} \leq \Delta I_L \left[ESR + \frac{1}{8fC_{OUT}} \right]$$

The output ripple will be highest at the maximum input voltage since ΔI_L increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirement. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR value. However, it provides lower capacitance density than other types. Although Tantalum capacitors have the highest capacitance density, it is important to only use types that pass the surge test for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR. However, it can be used in cost-sensitive applications for ripple current rating and long term reliability considerations. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input, V_{IN}. At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at V_{IN} large enough to damage the part.

Checking Transient Response

The regulator loop response can be checked by looking at the load transient response. Switching regulators take several cycles to respond to a step in load current. When a load step occurs, V_{OUT} immediately shifts by an amount equal to ΔI_{LOAD} (ESR) also begins to charge or discharge C_{OUT} generating a feedback error signal for the regulator to return V_{OUT} to its steady-state value. During this recovery time, V_{OUT} can be monitored for overshoot or ringing that would indicate a stability problem.

EMI Consideration

Since parasitic inductance and capacitance effects in PCB circuitry would cause a spike voltage on SW pin when high-side MOSFET is turned-on/off, this spike voltage on SW may impact on EMI performance in the system. In order to enhance EMI performance, there are two methods to suppress the spike voltage. One is to place an R-C snubber between SW and GND and make them as close as possible to the SW pin (see Figure 3). Another method

is adding a resistor in series with the bootstrap capacitor, C_{BOOT} . But this method will decrease the driving capability to the high-side MOSFET. It is strongly recommended to reserve the R-C snubber during PCB layout for EMI improvement. Moreover, reducing the SW trace area and keeping the main power in a small loop will be helpful on EMI performance. For detailed PCB layout guide, please refer to the section of Layout Consideration.

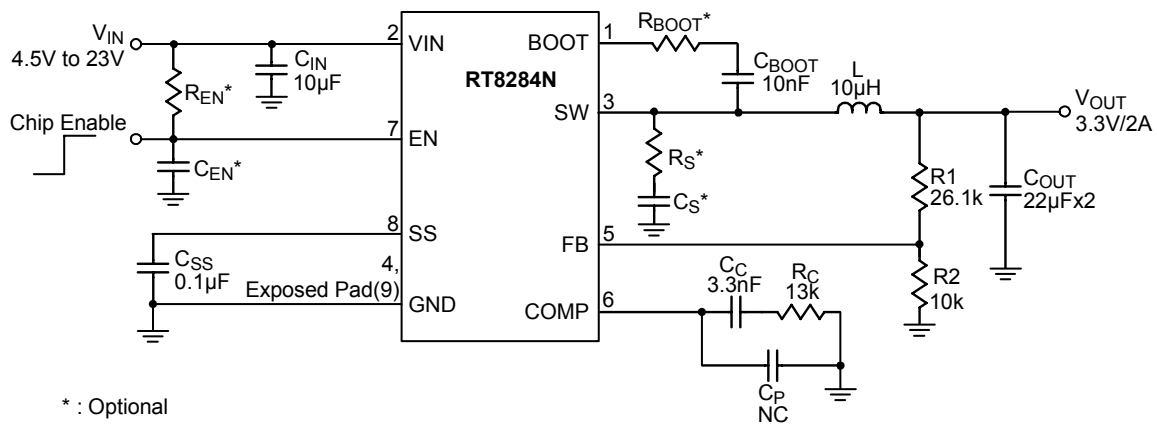


Figure 3. Reference Circuit with Snubber and Enable Timing Control

Thermal Considerations

For continuous operation, do not exceed absolute maximum operation junction temperature 125°C. The maximum power dissipation depends on the thermal resistance of IC package, PCB layout, the rate of surroundings airflow and temperature difference between junctions to ambient. The maximum power dissipation can be calculated by following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

Where $T_{J(MAX)}$ is the maximum operation junction temperature, T_A is the ambient temperature and the θ_{JA} is the junction to ambient thermal resistance.

For recommended operating conditions specification of RT8284N, the maximum junction temperature is 125°C. The junction to ambient thermal resistance θ_{JA} is layout dependent. For SOP-8 (Exposed Pad) package, the thermal resistance θ_{JA} is 75°C/W on the standard JEDEC 51-7 four layers thermal test board. For SOP-8 package, the thermal resistance θ_{JA} is 90°C/W on the standard JEDEC 51-7 four layers thermal test board. The maximum

power dissipation at $T_A = 25^\circ\text{C}$ can be calculated by following formula :

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (75^\circ\text{C/W}) = 1.33\text{W}$$

(min. copper area PCB layout with SOP-8 Exposed Pad)

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (49^\circ\text{C/W}) = 2.04\text{W}$$

(70mm² copper area PCB layout with SOP-8 Exposed Pad)

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (90^\circ\text{C/W}) = 1.11\text{W}$$

(min. copper area PCB layout with SOP-8)

The thermal resistance θ_{JA} of SOP-8 (Exposed Pad) is determined by the package architecture design and the PCB layout design. However, the package architecture design had been designed. If possible, it's useful to increase thermal performance by the PCB layout copper design. The thermal resistance θ_{JA} can be decreased by adding copper area under the exposed pad of SOP-8 (Exposed Pad) package.

As shown in Figure 4, the amount of copper area to which the SOP-8 (Exposed Pad) is mounted affects thermal

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performance. When mounted to the standard SOP-8 (Exposed Pad) pad (Figure 4.a), θ_{JA} is 75°C/W. Adding copper area of pad under the SOP-8 (Exposed Pad) (Figure 4.b) reduces the θ_{JA} to 64°C/W. Even further, increasing the copper area of pad to 70mm² (Figure 4.e) reduces the θ_{JA} to 49°C/W.

The maximum power dissipation depends on operating ambient temperature for fixed $T_{J(MAX)}$ and thermal resistance θ_{JA} . For RT8284N package, the Figure 5 of derating curves allows the designer to see the effect of rising ambient temperature on the maximum power dissipation allowed.

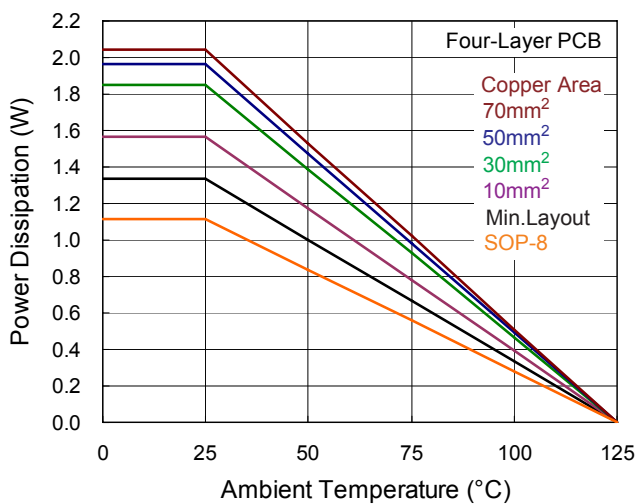
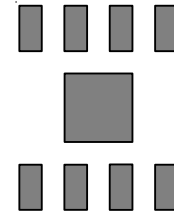
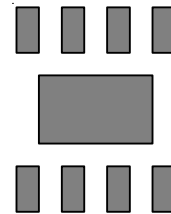


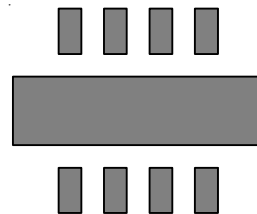
Figure 5. Derating Curves for RT8284N Package



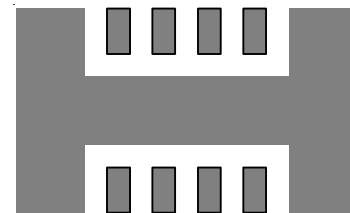
(a) Copper Area = (2.3 x 2.3) mm², θ_{JA} = 75°C/W



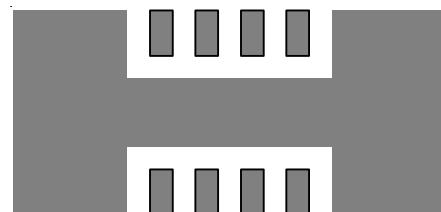
(b) Copper Area = 10mm², θ_{JA} = 64°C/W



(c) Copper Area = 30mm², θ_{JA} = 54°C/W



(d) Copper Area = 50mm², θ_{JA} = 51°C/W



(e) Copper Area = 70mm², θ_{JA} = 49°C/W

Figure 4. Thermal Resistance vs. Copper Area Layout Design

Layout Consideration

For best performance of the RT8284N, the follow layout giidelines must be strictly followed.

- ▶ Input capacitor must be placed as close to the IC as possible.
- ▶ SW should be connected to inductor by wide and short trace. Keep sensitive components away from this trace.
- ▶ The feedback components must be connected as close to the device as possible

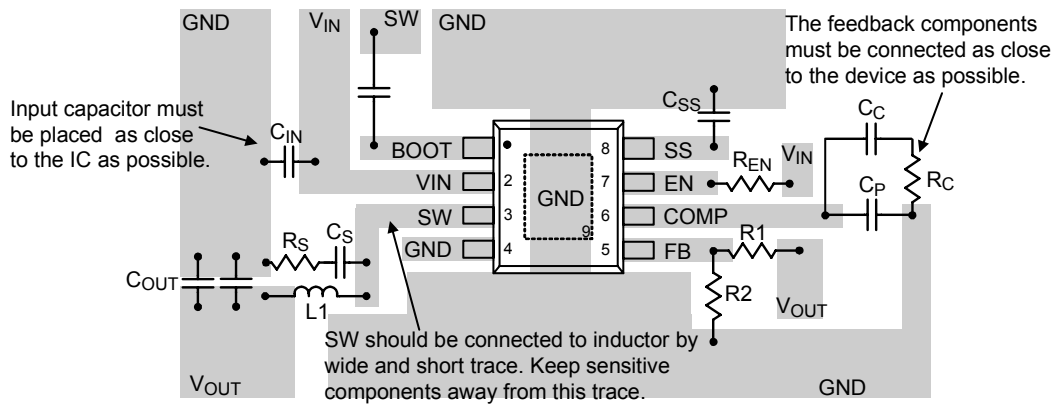


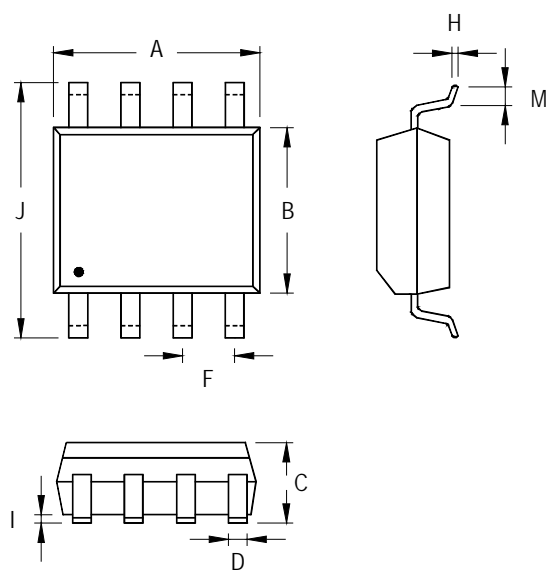
Figure 6. PCB Layout Guide

Table 3. Suggested Capacitors for C_{IN} and C_{OUT}

Location	Component Supplier	Part No.	Capacitance (μ F)	Case Size
C_{IN}	MURATA	GRM31CR61E106K	10	1206
C_{IN}	TDK	C3225X5R1E106K	10	1206
C_{IN}	TAIYO YUDEN	TMK316BJ106ML	10	1206
C_{OUT}	MURATA	GRM31CR60J476M	47	1206
C_{OUT}	TDK	C3225X5R0J476M	47	1210
C_{OUT}	MURATA	GRM32ER71C226M	22	1210
C_{OUT}	TDK	C3225X5R1C22M	22	1210

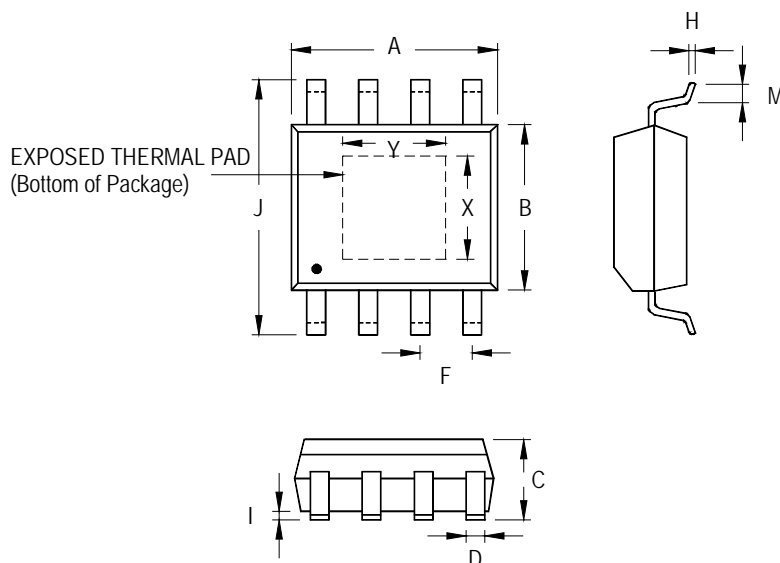
RT8284N

Outline Dimension



Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	4.801	5.004	0.189	0.197
B	3.810	3.988	0.150	0.157
C	1.346	1.753	0.053	0.069
D	0.330	0.508	0.013	0.020
F	1.194	1.346	0.047	0.053
H	0.170	0.254	0.007	0.010
I	0.050	0.254	0.002	0.010
J	5.791	6.200	0.228	0.244
M	0.400	1.270	0.016	0.050

8-Lead SOP Plastic Package



Symbol		Dimensions In Millimeters		Dimensions In Inches	
		Min	Max	Min	Max
A		4.801	5.004	0.189	0.197
B		3.810	4.000	0.150	0.157
C		1.346	1.753	0.053	0.069
D		0.330	0.510	0.013	0.020
F		1.194	1.346	0.047	0.053
H		0.170	0.254	0.007	0.010
I		0.000	0.152	0.000	0.006
J		5.791	6.200	0.228	0.244
M		0.406	1.270	0.016	0.050
Option 1	X	2.000	2.300	0.079	0.091
	Y	2.000	2.300	0.079	0.091
Option 2	X	2.100	2.500	0.083	0.098
	Y	3.000	3.500	0.118	0.138

8-Lead SOP (Exposed Pad) Plastic Package

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